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PASSAIC RIVER BASIN
TRIBUTARY TO ROCKAWAY RIVER
MORRIS COUNTY
NEW JERSEY

# COOKS POND DAM

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BACW61-79-C-0011

PHASE 1 INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM



DEPARTMENT OF THE ARMY

Philadelphia District Corps of Engineers Philadelphia, Pennsylvania

REAT. NO: DAEN | NAP- 53842 | NT 0=810-81 /07

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17. DISTRIBUTION STATEMENT (of the obstract entered in Block 20, If different from Report)

#### 18. SUPPLEMENTARY NOTES

Copies are obtainable from National Technical Information Service, Springfield, Virginia 22151.

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Dams Embankments National Dam Safety Program Cooks Pond Dam, N.J.

Seepage

Visual Inspection

Structural Analysis

Spillways Riprap

#### 20. ABSTRACT (Continue on reverse olds if necessary and identify by block number)

This report cites results of a technical investigation as to the dam's adequacy. The inspection and evaluation of the dam is as prescribed by the National Dam Inspection Act, Public Law 92-367. The technical investigation includes visual inspection, review of available design and construction records, and preliminary structural and hydraulic and hydrologic calculations, as applicable. An assessment of the dam's general condition is included in the report.

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# DEPARTMENT OF THE ARMY PHILADELPHIA DISTRICT, CORPS OF ENGINEERS CUSTOM HOUSE-2D & CHESTNUT STREETS PHILADELPHIA, PENNSYLVANIA 19106



Honorable Brendan T. Byrne Governor of New Jersey Trenton, New Jersey 08621

1 5 3000 1931

Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Cooks Pond Dam in Morris County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Cooks Pond Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in fair overall condition and the spillway is considered adequate. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

- a. Within one year from the date of approval of this report the following remedial actions should be initiated:
- (1) The spillway discharge chamber and discharge channel should be cleaned of debris.
- (2) Soil on the downstream side of the embankment should be properly graded, compacted and stabilized.
  - (3) Trees and adverse vegetation on the embankment should be removed.
  - (4) Deteriorated stoplogs should be replaced.
  - (5) Riprap on the upstream side of dam should be renovated.
  - (6) The crest of dam should be properly stabilized.
- (7) The observed seepage should be monitored on a periodic basis by a professional engineer experienced in the design and construction of dams in order to detect any changes in condition.

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NAPEN-N Honorable Brendan T. Byrne

- b. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam within one year from the date of approval of this report.
- c. An emergency action plan should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman Courter of the Thirteenth District. Under the provision of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

An important aspect of the Dam Inspection Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,

l Incl As stated

JAMES G. TON

Colonel, Corps of Engineers
Commander and District Engineer

Copies furnished:
Mr. Dirk C. Hofman, P.E., Deputy Director
Division of Water Resources
N.J. Dept. of Environmental Protection
P.O. Box CN029
Trenton, NJ 08625

Mr. John O'Dowd, Acting Chief Bureau of Flood Plain Regulation Division of Water Resources N.J. Dept. of Environmental Protection P.O. Box CM029 Trenton, NJ 08625

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#### COOKS POND DAM (NJ00810)

# CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 15 December 1980 and 12 March 1981 by Storch Engineers, under contract to the State of New Jersey. The State, under agreement with the U.S. Army Engineer District, Philadelphia, had this inspection performed in accordance with the National Dam Inspection Act, Public Law 92-367.

Cooks Pond Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in fair overall condition and the spillway is considered adequate. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

- a. Within one year from the date of approval of this report the following remedial actions should be initiated:
- (1) The spillway discharge chamber and discharge channel should be cleaned of debris.
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  - (3) Trees and adverse vegetation on the embankment should be removed.
  - (4) Deteriorated stoplogs should be replaced.
  - (5) Riprap on the upstream side of dam should be renovated.
  - (6) The crest of dam should be properly stabilized.
- (7) The observed seepage should be monitored on a periodic basis by a professional engineer experienced in the design and construction of dams in order to detect any changes in condition.
- b. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam within one year from the date of approval of this report.
- c. An emergency action plan should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

APPROVED: JAMES G. TON

Colonel, Corps of Engineers Commander and District Engineer

DATE: 15 Jun 1981

PHASE I REPORT

NATIONAL DAM SAFETY PROGRAM.

Name of Dam:

Cooks Pond Dam, NJ00810 /

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State Located:

New Jersey

County Located:

Morris

Drainage Basin:

Passaic River

Stream:

Tributary to Rockaway River

Dates of Inspection:

December 15, 1980

March 12, 1981

# Assessment of General Condition of Dam

Based on available records, past operational performance, visual inspections and Phase I engineering analysis, Cooks Pond Dam is assessed as being in fair overall condition.

Based on investigations of the downstream flood plain made in connection with this report, it is recommended that the hazard potential classification be downgraded from high to significant hazard.

The spillway is capable of passing the designated spillway design flood (100-year storm) without an overtopping of the dam and, therefore, is assessed as being adequate.

It is recommended that the following remedial measures be undertaken by the owner in the future:

- (1) The spillway discharge chamber and discharge channel should be cleaned of debris.
- 2) Soil on the downstream side of the embankment should be properly graded, compacted and stabilized.

- 3) Trees and adverse vegetation on the embankment should be removed.
- 4) Deteriorated stoplogs should be replaced.
- 5) Riprap on the upstream side of dam should be renovated.
- 6) The crest of dam should be properly stabilized.

The observed seepage should be monitored on a periodic basis by a professional engineer experienced in the design and construction of dams in order to detect any changes in condition.

In the future, the owner of the dam should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam.

Richard J. McDermott, P.E.

John E. Gribbin, P.E.



OVERVIEW - COOKS POND DAM

20 JANUARY 1981

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# PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of dam depends on numerous and constantly changing-internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that the unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydraulic and hydrologic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydraulic and hydrologic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

COOKS POND DAM, I.D. NJ00810

SECTION 1: PROJECT INFORMATION

# 1.1 General

# a. Authority

Public Law 92-367, August 8, 1972, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a National Program of Dam Inspection throughout the United States. The Division of Water Resources of the New Jersey Department of Environmental Protection (NJDEP) in cooperation with the Philadelphia District of the Corps of Engineers has been assigned the responsibility of supervising the inspection of dams within the State of New Jersey. Storch Engineers has been retained by the NJDEP to inspect and report on a selected group of these dams. The NJDEP is under agreement with the Philadelphia District of the Corps of Engineers.

### b. Purpose of Inspection

The visual inspections of Cooks Pond Dam were made on December 15, 1980 and March 12, 1981. The purpose of the inspections was to make a general assessment of the structural integrity and operational adequacy of the dam structure and its appurtenances.

# 1.2 Description of Project

#### a. Description of Dam and Appurtenances

The dam consists of an earth embankment with a spillway structure located near the center. The upstream face to the right of the spillway is formed by a concrete and stone masonry wall. The spillway consists of timber stoplogs fitted in a concrete headwall and discharges into an inlet chamber and then through two 18-inch concrete pipes and one 15-inch concrete pipe.

The elevation of the spillway crest is 528.0, National Geodetic Vertical Datum (N.G.V.D.) while that of the outlet invert is 521.8. The crest of the dam is at elevation 530.1 and the downstream channel bed is 521.8. The overall length of the dam is 443 feet and its height is 8.3 feet.

#### b. Location\_

Cooks Pond Dam is located in the Township of Denville, Morris County, New Jersey. Principal access to the dam is through a residential development which is entered from Diamond Spring Road at a point 1.7 miles north of N.J. Route 46. Discharge from the spillway of the dam flows into a tributary to the Rockaway River.

#### c. Size and Hazard Classification

The dam is classified in accordance with criteria presented in "Recommended Guidelines for Safety Inspection of Dams" published by the U.S. Army Corps of Engineers. Size categories consist of Small, Intermediate and Large while hazard categories are designated as Low, Significant and High.

<u>Size Classification:</u> Cooks Pond Dam is classified as "Small" size since its maximum storage volume is 99 acre-feet (which is less than 1000 acre-feet) and its height is 8.3 feet (which is less than 40 feet).

Hazard Classification: Visual inspection of the downstream flood plain of the dam together with breach analysis indicate that failure of the dam would not result in inundation of dwellings located within 3500 feet from the dam. Dam failure could cause damange to public roadways located 100 feet, 1500 feet and 3500 feet downstream from the dam. Accordingly, Cooks Pond Dam is classified as "Significant" hazard.

# d. Ownership

Cooks Pond Dam is privately owned by F.L. Petrozzo, Jr. and P.D. Palmer, P.O. Box 771, Bernardsville, N.J. 07924.

# e. Purpose of Dam

The purpose of the dam is the impoundment of a lake used for recreation.

# f. Design and Construction History

Cooks Pond Dam reportedly was constructed in or about 1945. Reportedly, no records or plans for the dam are on file.

### g. Normal Operational Procedures

The dam and its appurtenances are repaired on an "as needed" basis. The water level in the lake is partially lowered by means of stoplogs once or twice a year for maintenance purposes.

# 1.3 Pertinent Data

a.	Drainage Area	0.14 square miles
b.	Discharge at Damsite	
	Maximum flood at damsite	Unknown
	Outlet Works at pool elevation	40 cfs
	Spillway capacity at top of dam	44 cfs
с.	Elevation (N.G.V.D.)	
	Top of Dam	530.1
	Maximum pool-design surcharge	529.0
	Spillway crest	528.0
	Stream bed at toe of dam	521.8
	Maximum tailwater	524 (Estimated)
d.	Reservoir	
	Length of maximum pool	1200 feet (Estimated)
	Length of recreation pool	1000 feet (Scaled)
e.	Storage (Acre-feet)	
	Recreation pool	59 acre-feet
	Design surcharge	77 acre-feet
	Top of dam	99 acre-feet
ſ.	Reservoir Surface (acres)	
	Top of dam	20 acres (Estimated)
	Maximum pool – design surcharge	19 acres (Estimated)
	Recreation pool	17.5 acres

#### SECTION 2: ENGINEERING DATA

# 2.1 Design

No plans or calculations pertaining to the original design of the dam could be obtained.

# 2.2 Construction

No data or reports pertaining to the construction of the dam are available.

# 2.3 Operation

No data or reports pertaining to the operations of the dam are available.

# 2.4 Evaluation

# a. Availability

There is no available engineering data pertaining to the original construction of the dam.

# b. Adequacy

Available engineering data pertaining to Cooks Pond Dam is not adequate to be of significant assistance in the performance of a Phase I evaluation. A list of absent information is included in paragraph 7.1.b.

### c. Validity

The validity of engineering data cannot be assessed due to the absence of data.

#### SECTION 3: VISUAL INSPECTION

# 3.1 Findings

#### a. General

The inspections of Cooks Pond Dam were performed on December 15, 1980 and March 12, 1981 by staff members of Storch Engineers. A copy of the visual inspection check list is contained in Appendix 1. The following procedures were employed for the inspection:

- 1) The embankment of the dam, appurtenant structures and adjacent areas were examined.
- The embankment and accessible appurtenant structures were measured and key elevations determined by surveyor's level.
- 3) The embankment, appurtenant structures and adjacent areas were photographed.
- 4) The downstream flood plain was toured to evaluate downstream development and restricting structures.

#### b. Dam

Trees ranging in size from 2 inches to 12 inches were observed on the upstream and downstream sides of the embankment. The crest was generally grass covered with a pedestrian path located along its entire length. The concrete and stone masonry wall on the upstream side was in generally satisfactory condition. A one-foot gap between the wall and the spillway structure appeared to have been filled with rocks and mortar forming an unsatisfactory repair.

Riprap was observed along the upstream face to the left of the spillway. The stones had an average size of approximately 12 inches. The riprap was generally deteriorated.

Boulders were observed on the downstream side in the vicinity of the spillway structure. The boulders were haphazardly placed and did not appear to form a uniform slope stabilization. Voids in the soil behind the boulders were observed and sloughing of the embankment in the area of the boulders was noted. Evidence of loss of soil and insufficient compaction was also noted in the vicinity of the spillway.

On the downstream side of the dam, about 50 feet to the left of the spillway, an area of erosion was observed. The erosion appeared to be formed by pedestrian activity and surface runoff.

#### c. Appurtenant Structures

The spillway structure and discharge culverts appeared to be in generally satisfactory condition. However, a vertical crack about one-eighth inch wide was observed in one of the walls of the concrete chamber comprising the upstream portion of the spillway. The timber stoplogs fitted at the upstream end of the chamber were deteriorated. The chamber contained a significant accumulation of debris.

The concrete-lined discharge channel downstream from the dam was about half filled with leaves and rocks. It appeared to be in generally satisfactory condition.

#### d. Seepage

Water was discharging as a trickle from the right 18-inch culvert into the discharge channel. However, about 50 feet downstream, flow in the discharge channel had more quantity and contained orange colored deposits. The increased flow could indicate the emergence of seepage along the discharge channel.

#### d. Reservoir Area

The right side of the reservoir is wooded with homes along the shore, most of which are about 20 feet higher than the shoreline. A portion of the left side of the reservoir is a picnic area. All the land surrounding the reservoir is steeply sloping up from the reservoir, at grades of approximately 30 to 40 percent.

#### e. Downscream Channel

At the end of the discharge channel, a culvert crosses under a public roadway. Beyond the roadway, the downstream channel consists of a narrow pond with homesites located along both shores.

Approximately 1500 feet from the dam another public road crosses the channel. Downstream from the road, the channel continues as a natural stream with low banks and a flood plain about 100 feet wide.

#### SECTION 4: OPERATIONAL PROCEDURES

# 4.1 Procedures

The level of water in Cooks Pond is regulated by discharge over the stoplogs of the spillway and through the discharge culverts. The lake reportedly is partially lowered each year by removing stoplogs. At the time of inspection on December 19, 1980, the lake level was below the top of the stoplogs, whereas on March 12, 1981, the lake level was equal to the top of the stoplogs.

The stoplogs reportedly are not removed at times of storms to augment spillway capacity.

# 4.2 Maintenance of the Dam

Reportedly, maintenance of the dam is performed on an "as needed" basis.

# 4.3 Maintenance of Operating Facilities

Reportedly, maintenance of operating facilities is performed on an "as needed" basis.

# 4.4 Description of Warning System

Reportedly, no warning system is currently in use for the dam.

# 4.5 Evaluation of Operational Adequacy

The operation of the dam has been successful to the extent that the dam reportedly has not been overtopped.

Maintenance documentation is poor and maintenance has not been adequate in the following areas.

- 1) Trees on the embankment not removed.
- 2) Debris in the spillway chamber and discharge culvert not removed.
- 3) Deteriorated stoplogs not replaced.
- 4) Sloughing of downstream side of dam in vicinity of spillway not repaired.
- 5) Eroded area on downstream side of embankment not filled and stabilized.
- 6) Deteriorated riprap along upstream side of embankment not renovated.
- 7) Worn areas of embankment crest not stabilized.

#### SECTION 5: HYDRAULIC/HYDROLOGIC

#### 5.1 Evaluation of Features

#### a. Design Data

The quantity of storm water runoff that the spillway should be able to handle is based on the size and hazard classification of the dam. This runoff quantity, called the spillway design flood (SDF), is described in terms of return frequency or probable maximum flood (PMF) depending on the extent of the dam's size and potential hazard. According to the "Recommended Guidelines for Safety Inspection of Dams" published by the U.S. Army Corps of Engineers, the SDF for Cooks Pond Dam falls in a range of 100-year frequency to 1/2 PMF. In this case, the low end of the range, 100-year frequency, is chosen since the factors used to select size and hazard classification are on the low side of their respective ranges.

The SDF peak computed for Cooks Pond Dam is 175 c.f.s. This value is derived from the 100-year flood hydrograph computed by the use of the HEC-1-DAM Flood Hydrograph Computer Program using the Soil Conservation Service triangular unit hydrograph with curvilinear transformation. Hydrologic computations and computer output are contained in Appendix 4.

The spillway discharge rates were computed by the use of weir and orifice formulae appropriate for the configuration of the spillway as well as culvert capacity charts assuming inlet control. The total spillway discharge with lake level equal to the top of the dam was computed to be 44 c.f.s. The SDF was routed through the dam by use of the HEC-1-DAM computer program using the modified Puls Method. In routing the SDF, it was found that the dam crest would not be overtopped with 1.1 feet of freeboard remaining in a non-breach situation.

Accordingly, the subject spillway is assessed being adequate in accordance with criteria developed by the U.S. Army Corps of Engineers.

# b. Experience Data

Reportedly, the dam has never been overtopped. No damage to downstream structures has been reported.

# c. Visual Observation

No evidence of overtopping of the embankment was noted at the times of inspection.

### d. Overtopping Potential

According to the hydrologic and hydraulic analyses, a storm of intensity equivalent to the SDF will pass through the spillway without an overtopping of the dam and with a minimum freeboard of 1.1 feet.

#### e. Drawdown Data

Drawdown of the lake is accomplished by removing stoplogs in the spillway structure. Total time for drawdown is estimated to be 1.5 days. (See Appendix 4.)

#### SECTION 6: STRUCTURAL STABILITY

# 6.1 Evaluation of Structural Stability

#### a. Visual Observations

Seepage was observed in the discharge channel. Also, voids in the soil behind the boulders at the downstream end of the spillway discharge culvert were observed. The observed seepage and soil voids however, did not appear to be an indication of immediate structural instability.

#### b. Generalized Soils Description

The generalized soils Jescription of the dam site consists of stratified glacial drift deposited by melt water flowing from the Wisconsin glacier. The deposits are composed of sandy silt and gravel, with some silt and clay in depressions, overlying terminal moraines of the last Wisconsin glacial epoch as shown on the Geological Map of New Jersey. The ground moraine overlies a Pre-Cambrian formation (loose Gneiss).

#### c. Design and Construction Data

Analysis of structural stability and construction data for the embankment are not available.

#### d. Operating Records

No operating records are available for the dam. The water level of Cooks Pond is not monitored.

#### e. Post-Construction Changes

No changes to the dam or area around the dam are known to have occurred since the original construction of the dam in or about 1945.

# f. Seismic Stability

Cooks Pond Dam is located in Seismic Zone 1 as defined in "Recommended Guidelines for Safety Inspection of Dam" which is a zone of very low seismic activity. Experience indicates that dams in seismic Zone 1 will have adequate stability under seismic loading conditions if they have adequate stability under static loading conditions. Cooks Pond Dam appeared to be generally stable under static loading conditions at the times of inspection.

#### SECTION 7: ASSESSMENT AND RECOMMENDATIONS

### 7.1 Dam Assessment

#### a. Safety

Based on hydraulic and hydrologic analyses outlined in Section 5 and Appendix 4, the spillway of Cooks Pond Dam is assessed as being adequate. The spillway is able to pass the SDF without an overtopping of the dam.

The embankment appeared, at the time of inspection, to be generally stable. However, evidence of possible distress was observed. The evidence consisted of seepage and soil voids on the downstream side.

#### b. Adequacy of Information

Information sources for this report include 1) field inspections, 2) USGS quadrangle, 3) consultation with Mr. Frank Petrozzo the owner of the dam. The information obtained is sufficient to allow a Phase I assessment as outlined in "Recommended Guidelines for Safety Inspection of Dams."

Some of the absent data are as follows:

- 1. Construction and as-built drawings.
- 2. Description of fill material for embankment.
- 3. Design computations and reports.
- 4. Maintenance documentation.
- 5. Soils report for the site.
- 6. Post construction engineering reports.

#### c. Necessity for Additional Data/Evaluation

Although some data pertaining to Cooks Pond Dam are not available, additional data are not considered imperative for this Phase I evaluation.

# 7.2 Recommendations

#### a. Remedial Measures

Based on hydraulic and hydrologic analyses outlined in paragraph 5.1.a, the spillway is considered to be adequate.

It is recommended that the following remedial measures be undertaken by the owner in the future.

- 1) The spillway discharge chamber and discharge channel should be cleaned of debris.
- 2) Soil on the downstream side of the embankment should be properly graded, compacted and stabilized.
- Trees and adverse vegetation on the embankment should be removed.
- 4) Deteriorated stoplogs should be replaced.
- 5) Riprap on the upstream side of dam should be renovated.
- 6) The crest of dam should be properly stabilized.

# b. Maintenance

In the future, the owner of the dam should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam.

# c. Additional Studies

The observed seepage should be monitored on a periodic basis by a professional engineer experienced in the design and construction of dams in order to detect any changes in condition. <u>PLATES</u>

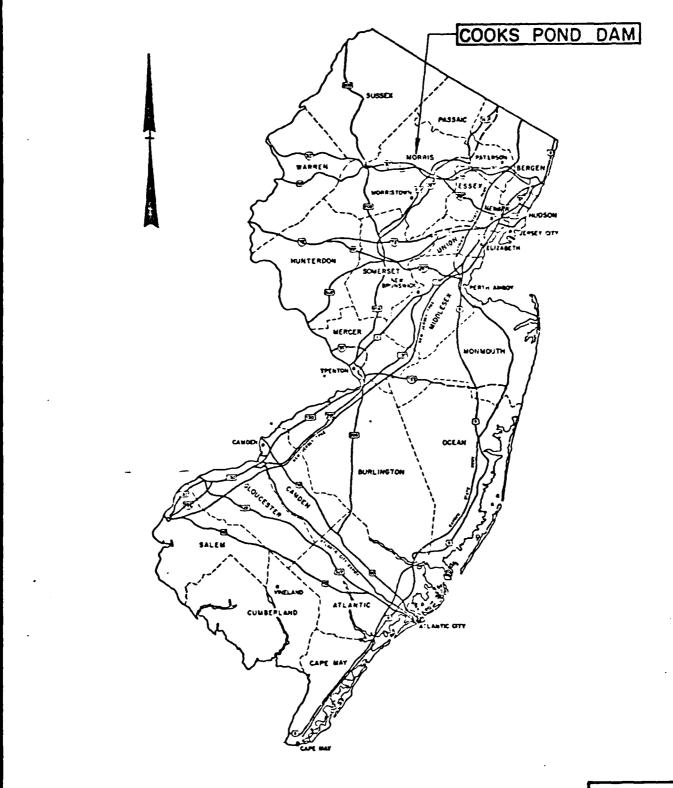


PLATE I

STORCH ENGINEERS
FLORHAM PARK, NEW JERSEY

DIVISION OF WATER RESOURCES
N.J. DEPT. OF ENVIR PROTECTION
TRENTON, NEW JERSEY

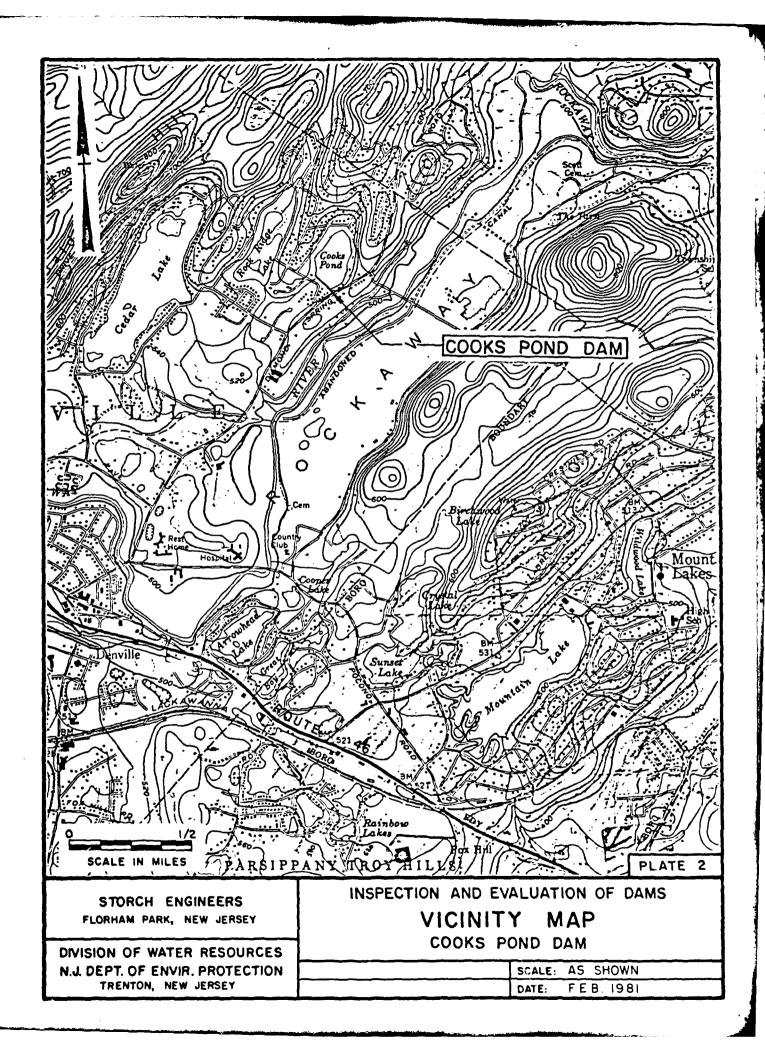
INSPECTION AND EVALUATION OF DAMS

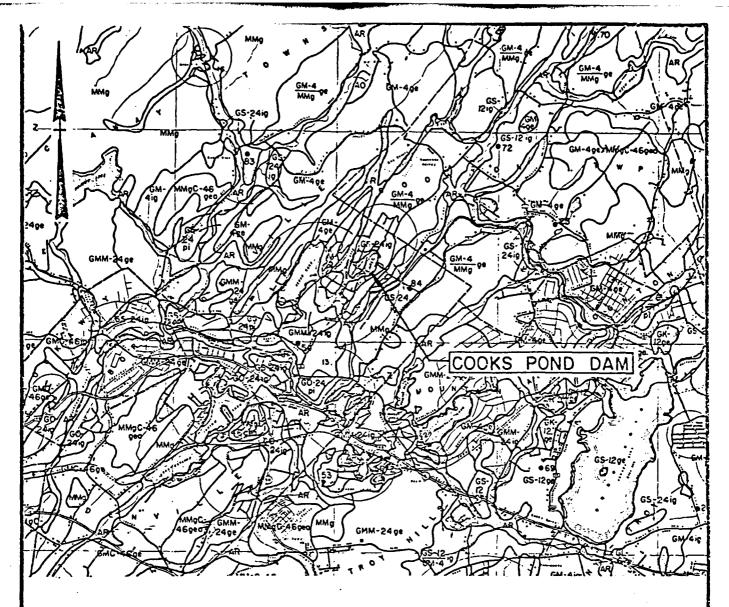
KEY MAP

COOKS POND DAM

SCALE: NONE

DATE: FEB. 198!





# Legend

GS-24

Silt, sandy silt, silty sand, gravelly sand, sandy gravel, gravel, and some clayey sand and gravel, overlying a terminal moraine of the Wisconsin glacial epoch.

Note:

Information taken from: Rutgers University Engineering Soil Survey of New Jersey, Report No. 9, Morris County, November 1953 and Geologic Map of New Jersey prepared by J. V. Lewis and H. Kummel 1910-1912, revised by H. B. Kummel 1931 and M. Johnson 1950.

PLATE 3

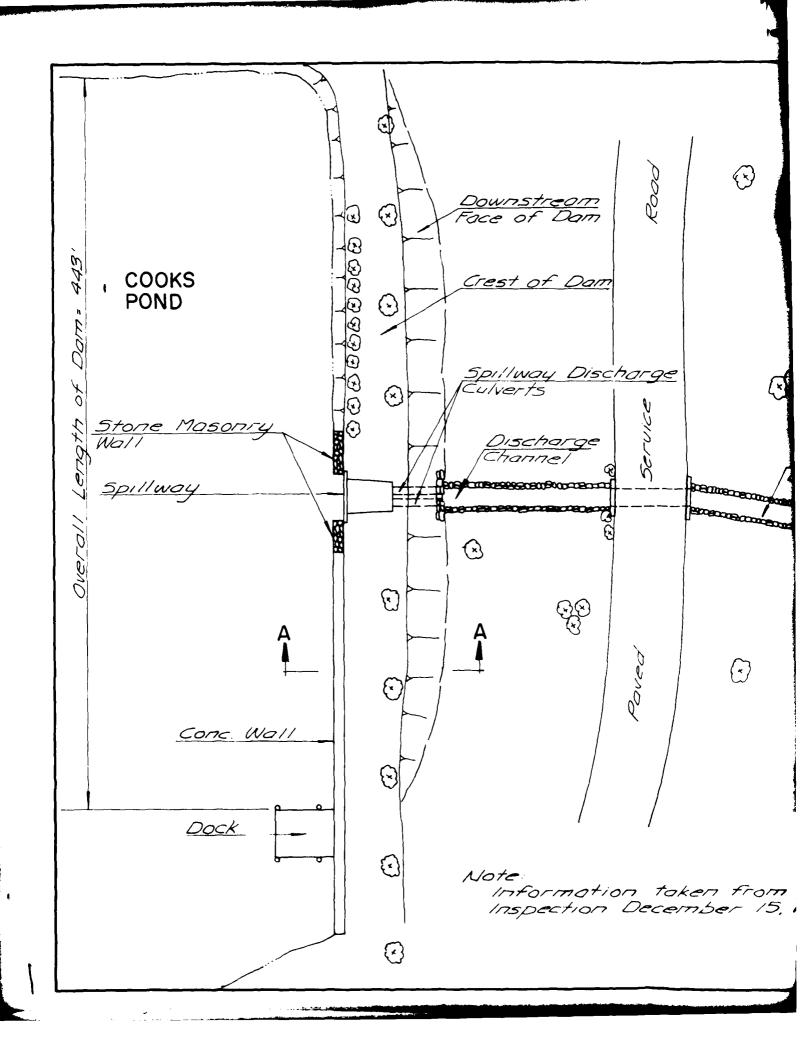
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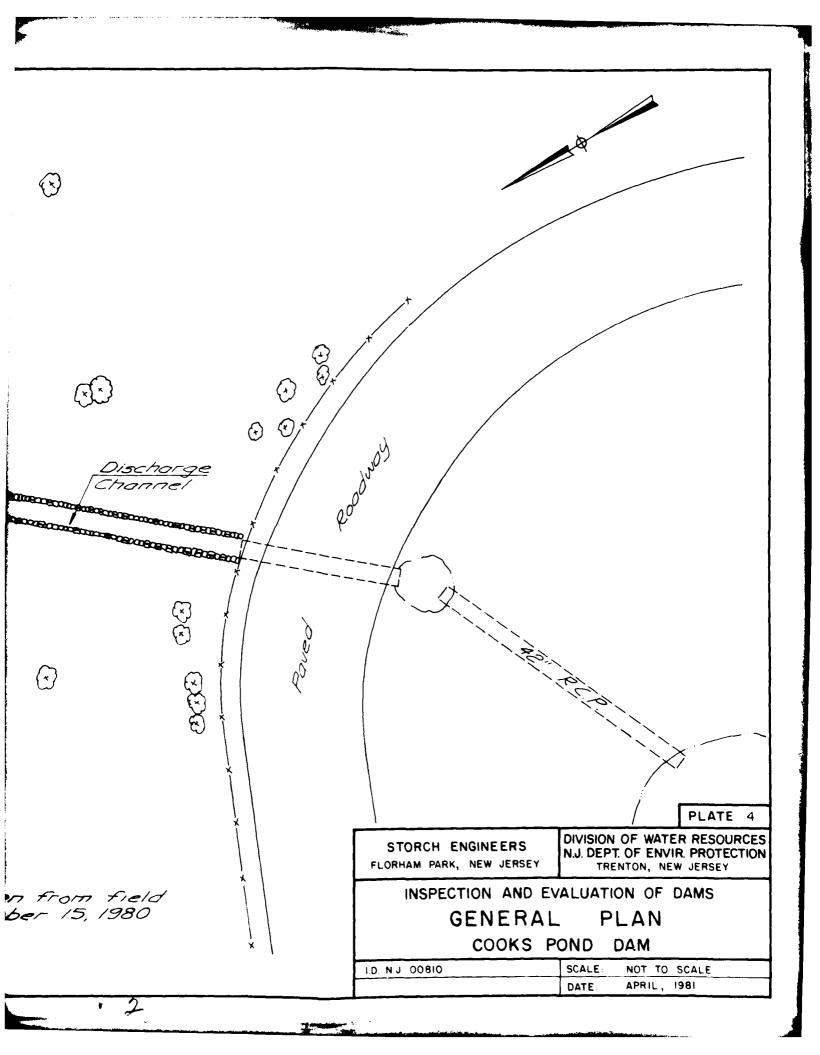
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TRENTON, NEW JERSEY

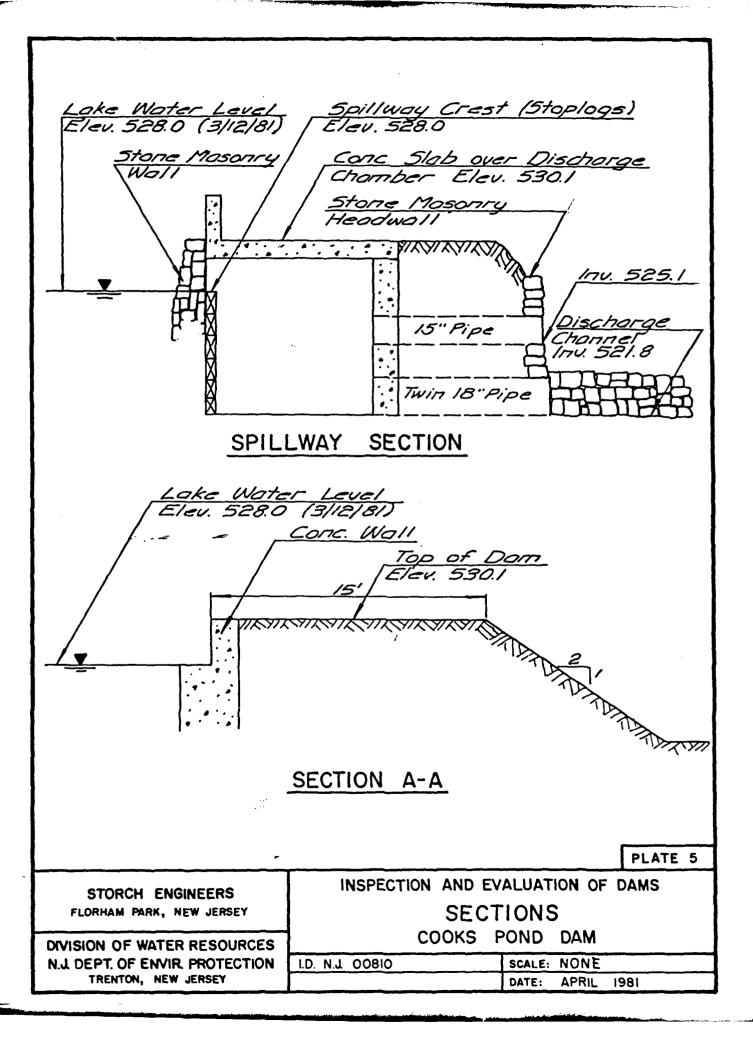
INSPECTION AND EVALUATION OF DAMS

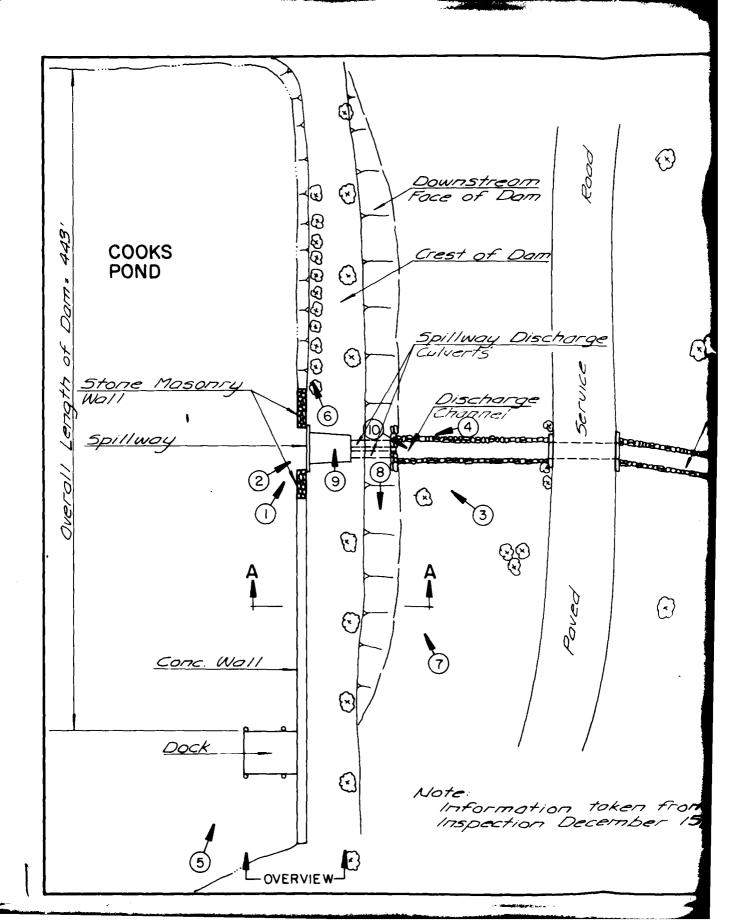
SOIL MAP COOKS POND DAM

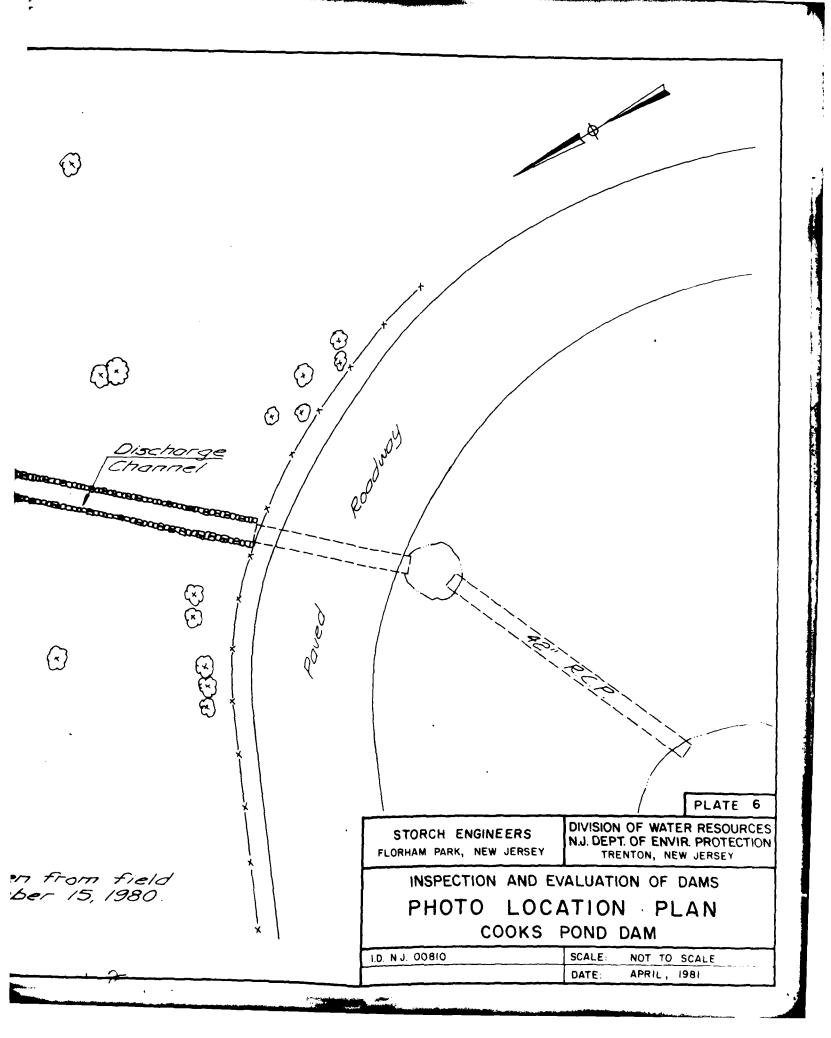
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#### APPENDIX 1

Check List - Visual InspectionCheck List - Engineering Data

Check List

Visual Inspection

Phase I

lame of Dam Cooks Pond Dam	County Morris	State N. J. Coordinators NADEP	
nate(s) Inspection 12/15/80, 3/12/81	Weather Cloudy	Temperature 20 <sup>0</sup> F.	
ຽວວໄ Elevatiດກ at time of Inspection <u> 528.0</u>	28.0 M.S.L.	Tailwater at Time of Inspection 520.6	_M.S.L
respection Personnel:	•		
Lu	Alex Nau Richard McDermott		
Daniel Buckelew	John Gribbin	Recorder	

### EMBANKMENT

	EMBANKMENT	
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
GENERAL	Crest covered with sparce grass, pedestrian path located along center. Trees (2" to 12") located on upstream and downstream sides. Concrete and stone masonry wall on upstream side in fair condition.	Trees should be removed. Crest should be stabilized.
· JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM	Generally sound. I foot wide gap between upstream wall and right side of spillway structure crudely filled with stones and mortar.	Gap between upstream wall and right side of spillway should be renovated.
ANY NOTICEABLE SEEPAGE	Evidence of seepage observed in concrete lined spillway discharge channel. Flow in channel 50' from dam greater than flow at dam. Also, orange colored deposits observed in flow 50' from dam. Difference in flow quantites could indicate seepage entering channel.	Seepage should be monitored.
STAFF GAGE AND RECORDER	None observed.	
DRAINS	None observed.	
	-	

# **EMBANKMENT**

# **OUTLET WORKS**

					•		1		ı	1		
	REMARKS OR RECOMMENDATIONS		•		•							
OUTLET WORKS	OBSERVATIONS	Same as spillway		1	ilmber stopiogs; same as spiliway weir.	Same as spillway		Same as spillway		Timber stoplogs; same as spillway weir.		
	VISUAL EXAMINATION OF	CONCRETE SURFACES IN	OUTLET CONDUIT		INTAKE STRUCTURE	OUTLET STRUCTURE		INNAUS FRIEIG			GATE AND GATE HOUSING	

### SPILLWAY

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
WEIR	Weir formed by timber stoplogs in deteriorated condition.	Stoplogs should be replaced.
		•
DISCHARGE CHAMBER	Concrete surfaces generally satisfactory. Vertical crack 1/8" wide observed on downstream wall of chamber. Interior of chamber contained significant accumulation of debris.	Debris should be removed.
DISCHARGE CULVERTS	Two 18-inch culverts with inverts at bottom of chamber appeared to have no reinforcing. One 15-inch culvert with invert above low level pipes appeared to be reinforced. Downstream ends of culverts stabilized by stone masonry headwall in satisfactory condition.	
DISCHARGE CHANNEL	Rectangular section concrete channel was generally: obscured by leave <b>s</b> and debris. Right lower culvert was discharging with a trickle into the channel.	Debris should be removed.

# INSTRUMENTATION

	INSTRUMENTALION	
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
MONUMENTATION/SURVEYS	None observed.	
. OBSERVATION WELLS	None observed.	•
WEIRS	None observed.	•
P1EZ0METERS	None observed.	
ОТИЕК	N. A.	•

### RESERVOIR

DE REMARKS OR RECOMMENDATIONS	Shores generally steeply sloping at grades of approx. 30% to 40%.	Unknown.	Right side of reservoir wooded with homesites along shore Dwellings about 20' above water level. Portion of left side consists of picnic area.	
VISHAL EXAMINATION OF		Unknown.	Right sic Dwellings STRUCTURES ALONG side cons BANKS	

# DOWNSTREAM CHANNEL

## CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION

REMARKS	•	Not available.	-	Not available.			Not available.	Not available.				Not available.	Not available.	Not available.
ITEM		DAM - PLAN . No	SECTIONS	SPILLWAY - PLAN NG	SECTIONS	DETAILS	OPERATING EQUIPMENT NO PLANS & DETAILS	OUTLETS - PLAN NG	DETAILS	CONSTRAINTS	DISCHARGE RATINGS	HYDRAULIC/HYDROLOGIC DATA No	RAINFALL/RESERVOIR RECORDS No	CONSTRUCTION HISTORY

Not available.

LOCATION MAP

		REMARKS
DESIGN REPORTS	Not available.	
GEOLOGY REPORTS	Not available.	
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM INSTABILITY SEEPAGE STUDIES	Not available.	
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD	Not available.	
POST-CONSTRUCTION SURVEYS OF DAM	Not available.	
BORROM SOURCES	Not available.	

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ITEM	REMARKS	
MONITORING SYSTEMS	Not available.	
MODIFICATIONS	Not available	
HIGH POOL RECORDS	Not available.	•
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	Not available.	
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	Not available.	
MAINTENANCE OPERATION RECORDS	Not available.	

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APPENDIX 2

Photographs

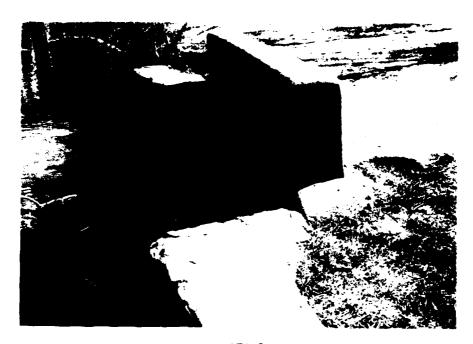


PHOTO 1
UPSTREAM END OF SPILLWAY



PHOTO 2
CREST OF SPILLWAY - TIMBER STOPLOGS



PHOTO 3

DOWNSTREAM SIDE OF DAM IN VICINITY OF SPILLWAY



PHOTO 4

DOWNSTREAM END OF SPILLWAY DISCHARGE CULVERTS



PHOTO 3

DOWNSTREAM SIDE OF DAM IN VICINITY OF SPILLWAY

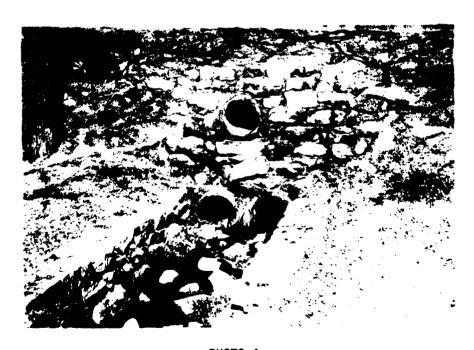


PHOTO 4

DOWNSTREAM END OF SPILLWAY DISCHARGE CULVERTS



PHOTO 5

CONCRETE WALL ALONG UPSTREAM SIDE OF DAM RIGHT OF SPILLWAY



PHOTO 6
EROSION ON UPSTREAM SIDE OF DAM LEFT OF SPILLWAY



PHOTO 7
DOWNSTREAM SIDE OF DAM



PHOTO 8
SOIL VOID ON DOWNSTREAM SIDE OF DAM NEAR SPILLWAY



PHOTO 9
CREST OF DAM SHOWING TOP OF SPILLWAY DISCHARGE CHAMBER



PHOTO 10
SPILLWAY DISCHARGE CHANNEL

APPENDIX 3

Engineering Data

#### CHECK LIST

#### HYDROLOGIC AND HYDRAULIC DATA ENGINEERING DATA

DRAINAGE AREA CHARACTERISTICS: <u>Suburban residential</u>
ELEVATION TOP NORMAL POOL (STORAGE CAPACITY): 528.0 (59 acre-feet)
ELEVATION TOP FLOOD CONTROL POOL (STORAGE CAPACITY): N.A.
ELEVATION MAXIMUM DESIGN POOL: 530.1
ELEVATION TOP DAM: 530.1
SPILLWAY CREST: Stoplogs in concrete intake structure
a. Elevation 528.0
b. Type Sharp crested weir
c. Width 0.2 foot
d. Length 5.0 feet
e. Location Spillover Upstream side of dam
f. Number and Type of Gates One set of stoplogs
OUTLET WORKS: Included in spillway structure
a. Type Timber stoplogs
b. Location Upstream end of spillway structure
c. Entrance Invert 521.8
d. Exit Invert 521.8
e. Emergency Draindown Facilities: Remove stoplogs
HYDOMETEOROLOGICAL GAGES: None
a. Type N.A.
b. Location N.A.
c. Records N.A.
MAXIMUM NON-DAMAGING DISCHARGE:
(Lake Stage Four) to Top of Dam) 44 - 5

#### APPENDIX 4

Hydraulic/Hydrologic Computations

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<u> </u>	PRECIPITAT	ION
; · ·	24 HOUR, 100-4E	AR RAINSTORM
	DISTRIBUTION FOR	COOKS POND DAM
<del></del>		
	TIME (HOUR)	RAIN (inches)
		0.075
	2	0,075
	3	0.075
	4	0.075
	5	0.075
	- 6-	0.075
		0,075
	8	0.075
	9	
		0.075 D.075
		0 075
	13	0.15
	14	0.15
	15	D:15
	16	0.33
	17	0.65
• · · -• ··	19	3,00
	19	0.65
<del>-</del>	20	0.33
	21	0.33
	22	0.15
	73	0.15
	24	0.15
	<u> </u>	7.09 inches

Project Cooks Pond Dam Made By JLP Date  Child By JE Date 3/3/8  THE SPILLWAY AT COOKS POND DAM CONSISTS OF A  SHARP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 10" AND ONE 15 Inch PIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Where:  Q = discharge over spillway  C = discharge coefficient  L = effective length of spillway  A = total head on spillway	STORCH ENGINEERS	Sheet <u>6</u> of <u>75</u>
THE SPILLWAY AT COOKS POND DAM CONSISTS OF A  SHARP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRY TWO 18" AND ONE 15 Inch DIAMETER  PIDE, DISCHARGE Q, CAN BE CALCULATED BY  Q = CL h 3/2  Where:  Or discharge piece willings	Project LOOKS YOND DAM	
THE SPILLWAY AT COOKS POND DAM CONSISTS OF A  SHARP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRY TWO 18" AND ONE 15 Inch DIAMETER  PIDE, DISCHARGE Q, CAN BE CALCULATED BY  Q = CL h 3/2  Where:  Or discharge piece willings		Chkd By <u>JG</u> Date <u>3/31/81</u>
THE SPILLWAY AT COOKS POND DAM CONSISTS OF A  SHARP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 18" AND ONE 15 Inch DIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Where:  Or displaced the Collings		
THE SPILLWAY AT COOKS POND DAM CONSISTS OF A  SHARP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 18" AND ONE 15 Inch DIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Where:  Or displaced the Collings		
THE SPILLWAY AT COOKS POND DAM CONSISTS OF A  SHARP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 18" AND ONE 15 Inch DIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Where:  Or displaced the Collings		
THE SPILLWAY AT COOKS POND DAM CONSISTS OF A  SHARP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 18" AND ONE 15 Inch DIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Where:  Or displaced the Collings	HYDRAULICS	
SHAPP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 18" AND ONE 15 Inch DIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Where:  D= displaces over college.		
SHAPP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 18" AND ONE 15 Inch DIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Where:  D= displaces over college.		
SHAPP CRESTED WEIR (STOPLOGS) AT THE ENTRANCE  TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 18" AND ONE 15 Inch DIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Where:  D= displaces over college.	THE SPILLWAY AT COOKS P	OND DAM CONSISTS OF A
TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 18" AND ONE 15 Inch DIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Q = CL & 3/2  Where:  O = discharge over collings		
TO AN INLET CHAMBER. THE CHAMBER DISCHARGES  THRU TWO 18" AND ONE 15 Inch DIAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Q = CL & 3/2  Where:  O = discharge over collings	SHARP- CRESTED WEIR (STOPLO	95) AT THE ENTRANCE
THRU TWO 18" AND ONE 15 Inch PLAMETER  PIPE, DISCHARGE Q, CAN BE CALCULATED BY  Q = CL & 3/2  Where:  O= desperse over collings		
PIDE, DISCHARGE Q, CAN BE CALCULATED BY $Q = CLh^{3}/2$ where: $Q = dsharer are sailings$	TO AN INLET CHAMBER. TI	HE CHAMBER DISCHARGES
PIDE, DISCHARGE Q, CAN BE CALCULATED BY $Q = CLh^{3}/2$ where: $Q = dsharer are sailings$		
$Q = cLh^{3}/2$ where: $Q = dshares executives$	THRU TWO 18" AND ONE	15 Inch DIAMETER
$Q = cLh^{3}/2$ where: $Q = dshares executives$		
where:	PIPE, DISCHARGE Q, CAN	BE CALCULATED BY
where:		<u> </u>
where:		
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where:	$Q = c \cdot l \cdot b \cdot 3 \cdot l$	
D= dispharer over sollingy	Y CLX	
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D= discharge over sollway	<u></u>	
D= dispharer over sollway		The second section of the second section of the second section of the second section s
D= dispharer over sollway	where:	
C = discharge coefficient  L = effective length of spillway  M = total head on spillway	D= dischar	ge over spillway
h= effective length of spillway. h=total head on spillway	C = discha	the coefficient
h=total head on spillway	L= effect	we length of spillway
	h = total	read on spillway
		O

Values for the discharge coefficient, "c" were taken from the "Handbook of Hydraulics" by King & Brater.

STORCH ENGINEERS	1 0 0	Sheet ot ot
Project	COOKS POND Dam	Made By Date
		Chkd By <i>JG</i> Date_ <i>3/31/8</i>
	TOP OF DAM	
	EL. = 530.1	
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	6.5: 5.4. 4 5.14.	4
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529.6		
	9.6' EL.=528.8	T00 1/5401/411
TOP OF STOPLOGS	79 ====================================	TOP HEADWALL
EL=528.0	4 1	EL.=527.90
		1
$\sqrt{I}$		
= 1	INV. 525.1	15" CONCRETE PIPE
5		
WATER ELEV.		STONE MASONRY P
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320.00	10	
	INV.521,8	18" CONCRETE
		18" CONCRETE
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STORCH ENGINEERS COOKS POND DAM		et_//_ of <u>/5</u>
Project CORS FOND DAM		Date 3-18-8
	Chkd By <u>JG</u>	_Date 3/31/81
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DRANDOWN CAPACIT	У	
-1-15" CONC. PIPE	<u> </u>	
/ TO CONC. FIFE	<del>5</del>	•
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STOP LOGS 2 HW-t.2		:
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Discharge based on culvert capac	ity charts.	
Maximum discharge, HW: 6.	. 2 '	
Q = 40 C.f.s.		
Average discharge, HW=3.	<u> </u>	
0: 2016		re de la companya de la colonia de la coloni
Q= 20 c.f.s.		
Drawdown		
		•
Drawdown Time = Storage Avg. Disci	at Spillway	
Avg. Disci	harge-Aug. Inflow	
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STORCH	ENGINEERS	COOKS POND DAM	Sheet <u>/2</u> of <u>/</u>
Project_		LUDRO TOND VAIII	Made By JLP Date 3-11-
			Chkd By Date
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<del></del>		BREACH ANALYSIS	
		71070	
	A BREA	CH HYDROGRAPH WILL	BE COMPUTED BY
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	PULS 1	METHOD. THE ASSUMED	BREACH CONDITIONS
	ARE A	s Follows:	
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		I. THE BREACH BEG SURFACE ELEVA	TION REACHES 528.9.
		2. TIME TO DEVELOP	BREACH = 1.0 HR.
		3. SECTION!	
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		FULLY DEVELOPED	BREACH
		10-29 DEVELOPED	UPC, 1011

STORCH ENGINE	Looks Pond D	_	She	et <u>14</u> of <u>1</u>
Project	LUOKS TOND U	am	Made By JLP	_Date 3-12-8
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END OF FEATH 3 CROSS SECTION

STA 34+00

STORCH ENGINEERS	Carlo D	10 Dam	- A	et <u>15</u> of <u>15</u>
Project	Cooks Por	ויאע עא	•	Date <u>3-11-81</u> Date <u>3/3//8/</u>
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RESULTS OF B	DEEACH:	<u> </u>		
Peak ou	tflow =	1508 c.f.	5.	
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Reach 3.	Max Stag	e 510.1		······································
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END OF REACH | CROSS SECTION

STA 3+35

HEC - 1 - DAM PRINTOUT

Overtopping Analysis

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NATIONAL DAM SAFETY PROGRAM	100. YEAR-SIDRH. ROULING	JOB SPECIFICATION  NO NUR NHIN IDAY  JOPER NWT LROPT TRACE  300 0 10 JOPER NWT LROPT TRACE	MULTI-PLAN ANALYSES NPLAN I NRTIDA	R1108 1.00		SUB-AREA RUNUT CONTOUR	RAPH T		INYDG IUHG TAREA SNAP TRSDA TRBPC RATIO ISNOU IBANE 1.0CAL 0 2 .10 0.00 0.000 0 1 0	LROPT BIRKR DLTKR RTIOL ERAIN BIRKS RTIOK BIRTL CHBIL ALGHX RTIHP 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	UNIT HYDROGRAPH DATA	RECESSION DATA STRIGE -1.00 DRCSN-05 RIIDRA-2.00	END-OF-PERIOD RAIN EXCS LOSS COMP.D AND.DA HR. HN. PERIOD RAIN EXCS LOSS COMP.D	8UM 7.11 4.33 2.78 1781.
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SUMMARY DF DAM SAFETY ANALYBIS   SUMMARY DF DAM SAFETY ANALYBIS   STALLAMY CREST TOP OF DAM   STALLAMY CREST TOP OF DAM   STALMAN HAXIMUM TIME   PLAN   STATION   19.67   19.67   10.00   17.   516.1   19.67   19.67   17.   516.1   19.67   19.67   19.67   17.   516.1   19.67	NITIAL VALUE   SPILLMAY CREST   TOP OF DAM	BUNHARY DF DAH SAFETY ANALYBIS  SUNHARY DF DAH SAFETY ANALYBIS  INITIAL VALUE SPILLWAY CREST TOP OF DAH  528.00	BUNHARY OF DAM SAFETY ANALYSIS  AL VALUE SPILLMAY CREST TOP OF DAM  28.00  59.  A4.  A4.  A4.  A4.  AA.  AA.  AA.  A
INITIAL VALUE   SPILLWAY CREST   TOP OF DAM     528.00	NITIAL VALUE   SPILLWAY CREST   TOP OF DAM   528.00   528.00   599.   99.	INITIAL VALUE   SPILLWAY CREST   TOP OF DAH	NATIAL VALUE   SPILLMAY CREST   TOP OF DAH
HAXIMUM HAXIMUM HAXIMUM DURATION TIME OF TIME  DEPTH. STORAGE GUTFLOW GVER TOP HAX. GUTFLOW FAILU  OVER DAM AC-FT CFS HOURS HOURS  O.00 19.67 0.0  RATIO FLOW.CFS STATION 2  FLAN 1 STATION 2  FLAN 1 STATION 2  HAXIMUM HAXIMUM TIME  RATIO FLOW.CFS STAGE.FT HOURS	HAXIMUM HAXIMUM HAXIMUM DURATION TIME OF TIME  DEPTH. STORAGE QUTFLOW GVER TOP HAX. OUTFLOW FAILU  OVER DAM AC-FT CFS HOURS HOURS  PLAN 1 STATION 1  PLAN 1 STATION 2  FLAN 1 STATION 2  HAXIMUM HAXIMUM TIME  RATIO FLOW,CFS STATION 2  1.00 17. 516.1 19.67  FLAN 1 STATION 2  HAXIMUM HAXIMUM TIME  RATIO FLOW,CFS STAGE,FT HOURS  1.00 17. 510.1 19.83	HAXIMUM HAXIMUM HAXIMUM DURATION TIME OF TIME  DEPTH. STORAGE QUITCOM GOVER TOP HAX. OUTFLOW FAILU  OVER DAM AC-FT CFS HOURS HOURS  DO.OO 17. 12. 0.00 19.67  HAXIMUM HAXIMUM TIME  RATIO FLOW.CFS STATION 2  HAXIMUM HAXIMUM TIME  RATIO FLOW.CFS STATION 3  1.00 17. 510.1 19.83	MAXIMUM MAXIMUM HAXIMUM DURATION TIME OF TIME  DEPTH. STORAGE OUTFLOW OVER TOP HAX OUTFLOW FAILU  OVER DAM AC-FT CFS HOURS HOURS  0.00 17. 12. 0.00 19.67  1.00 17. 516.1 19.67  PLAN 1 STATION 2  PLAN 1 STATION 2  PLAN 1 STATION 3  PLAN 1 STATION 3
PLAN 1 STATION 1  RATIO FLOW.CFS STATION 2  PLAN 1 STATION 2  PLAN 1 STATION 2  RATIO FLOW.CFS STAGE, THE	PLAN 1 STATION	PLAN 1	PLAN 1
HAXIMUM MAXIMUM FLOWLCFS BIAGE, FT H 17. S16.1 1 PLAN 1 STATION 2 HAXIMUM MAXIMUM FLOWLCFS STADE, FT H	HAXIMUM HAXIMUM FLOW.CFS BIAGE,FT H 17. 516.1 1 PLAN 1 BTATION 2 HAXIMUM HAXIMUM FLOW.CFB BIAGE,FT H 17. 510.1 1	HAXIMUM MAXIMUM FLOW.CFS BIAGE,FT H 17. S16.1 1 PLAN 1 STATION 2 HAXIMUM MAXIMUM FLOW.CFS STAGE,FT H 17. S10.1 1	HAXIMUM HAXIMUM ELOW.CFS BIAGE, FI  17. S16.1  PLAN 1 STATION 2  HAXIMUM HAXIMUM FLOW, CFS STATION 3  PLAN 1 STATION 3 FLOW, CFS STATION 3
PLAN 1 STATION 2 HAXIMUM HAXIMUM FLOWICFS STAGE,FT H	17. 516.1 1 PLAN 1 8TATION 2 HAXIMUM HAXIMUM FLOW,CF8 8TAGE,FT H 17. 510.1 1	LAN 1 8TATION 2  HAXIMUM HAXIMUM FLOW,CF8 8TAGE,FT H  17. 510.1 1	LAN 1 BTATION 2 HAXIMUM HAXIMUM FLOW,CFB BTAGE,FT 17. 510.1 CAN 1 BTATION 3 FLOW,CFB BTAGE,FT FLOW,CFB BTAGE,FT
HAXIMUM MAXIMUM FLOW, CF8 81AGE, FT H	HAXIHUM HAXIHUM FLOW, CFB 8TAGE, FT H	HAXIHUM   HAXIHUM	HAXIMUM HAXIMUM FLOW,CFB BTAGE,FT 17. 510.1 ILAN 1 BTATION 3 FLOW,CFB BTAGE,FT
HAXIMUM MAXIMUM FLOW,CFB BTAGE,FT H	HAXIMUM HAXIMUM FLOW,CF8 8TAGE,FT H 17. 510.1 1	HAXIMUM HAXIMUM FLOW,CFB 8TAGE,FT H 17, 510.1 1	HAXIMUM HAXIMUM FLOW,CFB STAGE,FT 17. 510.1  **LAN 1 STATION 3 FLOW,CFS STAGE,FT
	17. 510.1	17. 510.1 PLAN 1 BTATION 3	PLAN 1 STATION 3 FLOW, CFS STABE, FT

HEC - 1 - DAM PRINTOUT

Breach Analysis

1A1 A2					DAK SAFE' D. NEW J		AM		<del></del>	
_A3_			10		SIORH RO					<u> </u>
В	300	0	10				0	0	4	
B1	5									
1_	1_	1_	1		_ <del></del>		<del></del>	<del></del>		
J1	1									
K	0	LAKE			0	0	2			
_K1_		INELOW	<u>HYDROGRA</u> I	0 <u>1_01</u>	OKS POHD	MAG				
н	0	2	0.1		0.1	0			1	
0	144									
-010	.0125_	_0.0125_	_0.0125_	-0.0125	0.0125_	0.0125	_C.0125	0.0125_	0.0125_	0.0125
010	.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125
010	.0125	0.0125	0.0125	0.0125	0.0125	0.0125			0.0125	0.0125
010	0.0125_	_0.0125_	_0.0125_	_0.0125_	_0.0125_	_0.0125_	_0.0125_	_0.0125_	_0.0125_	_0.0125
010	.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	0.0125	(.0125	0.0125
		0.0125		0.0125	0.0125	0.0125			0.0125	0.0125
_010	0.0125_	_0.0125_	_0.0125_	_0+0125_	_0.0125_	_00125	_0.0125.	_0.0125_	_0.0125_	
010	0.0125	0.0125	0.025	0.025	0.025	0.025	0.025	0.025	0.025	0.025
01	0.025	0.025	0.025	0.025	0.025	0.025	0.025	0.025	0.025	0.025
_01_	0.055	0.055_	0.055	0.055_	0.055	0.055_	0.11	0.11_	0.11	0.11
01	0.11	0.11	0.5	0.5	0.5	0.5	0.5	0.5	0.11	0.11
01	0.11	0.11	0.11	0.11	0.055	0.055	0.055	0.055	0.055	0.055
_ 01	-0.055-	0.055_	0+055_	0-055-	0.055_	0055-	0.025_	0.025_	0.025_	0.025
01	0.025	0.025	0.025	0.025	0.025	0.025	0.025	0.025	0.025	0.025
01	0.025	0.025	0.025	0.025						
·- Ŧ -							1+5_	0-15		
W2		0.36								
X	-1.0	-0.05	2.0							
K -	1	DAH-								
K1		ROUTE	DISCHARG	E THRU D	MA					
Υ				1	1	-				
_Y1-							528.0-	1_		
Y4	528.0	528.5	529.0	529.6	530.0	531.0	532.0	533.0	534.0	535.0
Y 5		6	16.8	34.4	42.2	57.1	68.9	77.0	85.0	90.0
\$A		17-45_		38.11-						
\$E	520	527	540	260						
	528.0									
	_530.1_	2.63_	1.5	443_			<del></del>			
\$ B	100	1	521.8	1.0	528.0	528.9	_			
K	1	1	· - · · · ·		,		1			
		HANNEL—F	A-BHITUOS				<del></del>	<del></del> -	·	<del></del>
Y				1	1					
-Y1	1									
-¥6		<del>0-035</del> -		- 516.0				F11 C		844 4
Y7		525.9	35	522.4	75	518.5	100	516.0	140	516.0
Y7		521.5	200	324.2	220	526.9				
K	1,	2		EACH A			. 1			
K1 Y		DENNEL P	ROUTING R	-	_					
				1	1					
Y1	1	0 075	۸.	E10 0	<b>570</b> •					
Y 6 Y 7		0.035 530	0.1 50		530.0	1165 523		E1A	254	FIA
				525 	100 - <del>1</del> 00-		150	510	250	510
_	1	3			700-		1			
K1	-	_	ROUTING R	E UTAT			•			
		, HINNEL P	CONTINU K	ENCH 3						
- ¥ -	1									
17		0.035	0.1	502	512	1900	0.004			
7 0	-	- 520.5						502	425	502
• •	435	512	835	514.5		517				
,	**									

HYDROBKARH - NOULTING	SOUTE DISCHARGE THRU DAM

		-	00 534.00 535.00	.00 B3.00 80.00					
IAUTO			533.00	72.00					
NHE ISTAGE	0	LBIR 0 0 ATORA ISPRAT		68.90			EXPL 0.0		FAILEL 528.90
}	1	1949	00000	57.10			COOL CAREA	DANNIB.	HEEL 528.00
	190	1001	0.00°	530,00			0+0 ELEVL	DOD EXPD.	ACH. DAT
	ITAPE 0 TIME DATA		0.000 0.000	n			EXPU EL	CODD 2.6	DAM BREACH DATA ELBH TFAIL 521,80 1.00
	IECON	IREB 1	LAG	34.40	38.	1045	4 (	TOPEL	
DE THRU DAM	1 COMP	AVB 0.00	NBT DL	529.00	31.	353.	SPW10 C		BRHID 100.
ROUTE DISCHARGE T	ISTAU	00000	NSTPB		17.	41.	\$22. CREL 8(		
ROUTE		0.00		528,50					
				97ABE 528.00	BURFACE AREA 0.	CAPACITY	EL EVATIONA 520.		

BEGIN DAN FAILURE AT 18.67 HOURS

PEAK. OUTFLOW 19----1508.AT. TIME \_19.46.HOURS\_\_

				•				٠	
HYDROGRAPH AT	LAKE	.10	-	175.					
ROUTED TO	DAH	.10		1486.					
ROUTED TO	1	.10	-	1504.					
ROUTED TO	2	.10		1481.					
ROUTED TO	F .	.10		1457.					
1				ins.	BUHHARY OF DA	DAM SAFETY ANAL	ANALYB18		
PLAN 1 .		:	ELEVATION	INITIAL VALUE 528.00		SPILLWAY CREST 528.00	104	0F DAM 530.10	
		OUTFLOW	107		ò	0		7.	
	RATIO OF PMF	MAXIMUM RESERVOIR	AUN JOIR ILEU	MAXINUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FI	HAXIHUH OUTFLOW CF8	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TINE OF FAILURE HOURS
	1.00	528.94	.94	00.0	76.	1508.	0.00	19.46	18.67
				14	PLAN 1	STATION	1		
				RATIO	HAXIHUH FLOW, CFB	HAXIMUH BIAGE,FI	TIME		
				1.00	1504.	518.7	19.50		
				14	PLAN 1	BTATION	2		
				RATIO	FLOWICES	BTAGE, FT	TIME		
				1.00	1481-	512.5	19.50		
				I	PLAN. 1	BIATION	-		
				RATIO	HAXINUH ELOW, CFB	HAXIHUH BIAGE, EL	TIME		
		•••••		1.00	1457.	510.1	19.50		

APPENDIX 5

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